



# 3次元カセーシ流れについて

## 内容

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# 1. 運動方程式, 境界条件, 境界力

カセーニ流の運動方程式は

$$U \frac{\partial u_j}{\partial x_1} = -\frac{1}{\rho} \frac{\partial p}{\partial x_j} + \nu \nabla^2 u_j, \quad j=1,2,3, \quad (1.1)$$

( $\nu = \mu/\rho$ )

連続の方程式は

$$\sum_j \frac{\partial u_j}{\partial x_j} = 0, \quad (1.2)$$

(1.1) と (1.2) より

$$\nabla^2 p = 0, \quad (1.3)$$

(1.1) の  $U$  の符号を変えると 随伴方程式が得られ, その解は一般流れを逆にしたものと考えられるから以下 逆流れと呼び (1.1) 印でこれを示すものとする。

$$-U \frac{\partial \tilde{u}_j}{\partial x_1} = -\frac{1}{\rho} \frac{\partial p}{\partial x_j} + \nu \nabla^2 \tilde{u}_j, \quad (1.4)$$

$$\sum_j \frac{\partial \tilde{u}_j}{\partial x_j} = 0, \quad (1.5)$$

境界条件は 物体表面  $S$  上で

$$u_1 = -U, \quad u_2 = u_3 = 0, \quad \text{on } S, \quad (1.6)$$

$$\tilde{u}_1 = U, \quad \tilde{u}_2 = \tilde{u}_3 = 0, \quad \text{on } S, \quad (1.7)$$

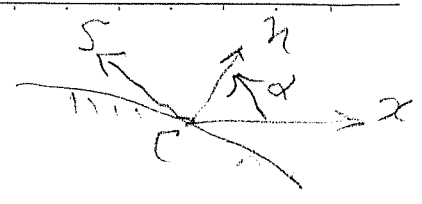
軸対称流れでは

$$x_1 = x, \quad x_2 = r \cos \theta, \quad x_3 = r \sin \theta, \quad (1.8)$$

円筒座標を導入し

$$\left. \begin{aligned} u_r &= u_2 \cos \theta + u_3 \sin \theta \\ v_\theta &= -u_2 \sin \theta + u_3 \cos \theta \end{aligned} \right\} \quad (1.9)$$

同様の曲線を  $C$  とし  $\alpha$  を  $\Gamma$  の傾き



定義すると  $U$  の法線成分  $U_n$ ,

切線成分  $U_s$  は.

$$\begin{aligned} U_n &= U_1 \cos \alpha + U_2 \sin \alpha \\ U_s &= -U_1 \sin \alpha + U_2 \cos \alpha \end{aligned} \quad \dots (1.10)$$

(1.6), (1.7) を法線成分と切線成分で表わすと上式より

$$\begin{aligned} U_n &= -U \cos \alpha = -U \frac{\partial x}{\partial n} = -U \frac{\partial \Gamma}{\partial s} \\ U_s &= U \sin \alpha = +U \frac{\partial \Gamma}{\partial n} = -U \frac{\partial x}{\partial s} \end{aligned} \quad \dots (1.11)$$

もう一度一般的記号に代って法線の方向余弦を  $(l_j)$

とするとその面に働く流体力の各成分  $\tau_j$  は

$$\tau_j = \sum_{i=1}^3 \tau_{ji} l_i \quad (1.12)$$

$$\tau_{ji} = \mu \gamma_{ji} - p \delta_{ij} \quad (1.13)$$

$$\gamma_{ji} = \gamma_{ij} = \frac{\partial u_j}{\partial x_i} + \frac{\partial u_i}{\partial x_j} \quad (1.14)$$

今温度  $\zeta_j$  を導入しよう。

$$\zeta_j = \frac{\partial u_{j+2}}{\partial x_{j+1}} - \frac{\partial u_{j+1}}{\partial x_{j+2}} \quad (1.15)$$

$j+2$  は  $\text{mod}(3)$  で  $u_j$  に等しいと解釈する。

$$\zeta_1 = \frac{\partial u_3}{\partial x_2} - \frac{\partial u_2}{\partial x_3}, \quad \zeta_2 = \frac{\partial u_1}{\partial x_3} - \frac{\partial u_3}{\partial x_1}, \quad \zeta_3 = \frac{\partial u_2}{\partial x_1} - \frac{\partial u_1}{\partial x_2}$$

(1.1) から

$$\begin{aligned} U \frac{\partial}{\partial x} \zeta_j &= \nu \nabla^2 \zeta_j \\ -U \frac{\partial}{\partial x} \bar{\zeta}_j &= \nu \nabla^2 \bar{\zeta}_j \end{aligned} \quad (1.16)$$

である。

さて物作表面上で (1.6) が成立するとすれば、表面の速度を  $U$  に代って微分すれば 0 であるから

$$\frac{\partial U_j}{\partial x_i} = \frac{\partial U_j}{\partial x} l_i, \quad (1.17)$$

(1.15) に代入すると

$$\zeta_j = \frac{\partial U_{j+1}}{\partial x} l_{j+1} - \frac{\partial U_{j+1}}{\partial x} l_{j+2}, \quad (1.18)$$

また (1.2) から

$$\sum_{i=1}^3 \frac{\partial U_j}{\partial x_i} l_i = 0, \quad (1.19)$$

$$\therefore \frac{\partial U_j}{\partial x} = \zeta_{j+1} l_{j+2} - \zeta_{j+2} l_{j+1}, \quad (1.20)$$

これを (1.14) に代入すると

$$\begin{aligned} \sum_i \sigma_{ij} l_i &= \frac{\partial U_j}{\partial x} + l_j \sum_i \frac{\partial U_i}{\partial x} l_i \\ &= \zeta_{j+1} l_{j+2} - \zeta_{j+2} l_{j+1}, \quad (1.21) \end{aligned}$$

よって

$$\tau_j = -p l_j + \mu [\zeta_{j+1} l_{j+2} - \zeta_{j+2} l_{j+1}], \quad (1.22)$$

法線成分は

$$\tau_n = \sum_j \tau_j l_j = -p \quad (1.23)$$

∴ 再び軸対称な流れを考へ

$$\left. \begin{aligned} \tau_r &= \tau_2 \cos \theta + \tau_3 \sin \theta \\ 0 &= -\tau_2 \sin \theta + \tau_3 \cos \theta \end{aligned} \right\} \quad (1.24)$$

$$\left. \begin{aligned} \tau_2 \cos \theta + \tau_3 \sin \theta &= 0 \\ -\tau_2 \sin \theta + \tau_3 \cos \theta &= \zeta \end{aligned} \right\} \quad (1.25)$$

と仮くと  $\left( \begin{aligned} l_2 \cos \theta + l_3 \sin \theta &= \sin \alpha \\ l_1 &= \cos \alpha \end{aligned} \right)$

$$\left. \begin{aligned} \tau_1 &= -p \cos \alpha - \mu \zeta \sin \alpha \\ \tau_r &= -p \sin \alpha + \mu \zeta \cos \alpha \end{aligned} \right\} \quad (1.26)$$

法線成分と切線成分は整理すると

$$\left. \begin{aligned} \tau_n &= \tau_1 \cos \alpha + \tau_r \sin \alpha = -p \\ \tau_s &= -\tau_1 \sin \alpha + \tau_r \cos \alpha = \mu \zeta \end{aligned} \right\} \quad (1.27)$$

特に

$$\begin{aligned} \frac{\partial u_1}{\partial x_1} &= \frac{\partial u_1}{\partial x} l_1 = (l_2 l_3 - l_3 l_2) l_1 \\ &= \zeta (l_3 \sin \theta + l_2 \cos \theta) l_1 = -\zeta \sin \alpha \cos \alpha \quad (1.28) \end{aligned}$$

$$\gamma_{ij} \Big|_S = \frac{\partial u_i}{\partial x_i} + \frac{\partial u_i}{\partial x_j} = \frac{\partial u_i}{\partial n} l_i + \frac{\partial u_i}{\partial n} l_j$$

$$= (\gamma_{j+1} l_{j+2} - \gamma_{j+2} l_{j+1}) l_i + (\gamma_{i+1} l_{i+2} - \gamma_{i+2} l_{i+1}) l_j$$

$$\sum_j \sum_i \gamma_{ij} \tilde{\gamma}_{ij} \Big|_S = \sum_i \sum_j \left[ (\gamma_{j+1} l_{j+2} - \gamma_{j+2} l_{j+1}) (\tilde{\gamma}_{j+1} l_{i+2} - \tilde{\gamma}_{j+2} l_{j+1}) l_i^2 \right. \\ \left. + (\gamma_{i+1} l_{i+2} - \gamma_{i+2} l_{i+1}) (\tilde{\gamma}_{i+1} l_{j+2} - \tilde{\gamma}_{i+2} l_{i+1}) l_j^2 \right. \\ \left. + 2(\gamma_{i+1} l_{j+2} - \gamma_{j+2} l_{j+1}) (\tilde{\gamma}_{i+1} l_{i+2} - \tilde{\gamma}_{i+2} l_{i+1}) l_i l_j \right]$$

$$= 2 \sum_j \left[ \gamma_{i+1} \tilde{\gamma}_{j+1} l_{j+2}^2 + \gamma_{j+2} \tilde{\gamma}_{j+2} l_{j+1}^2 \right. \\ \left. - \gamma_{j+2} \tilde{\gamma}_{j+1} l_{j+1} l_{j+2} - \gamma_{i+1} \tilde{\gamma}_{i+2} l_{j+1} l_{j+2} \right]$$

$$+ 2 \sum_i \sum_j \left[ \gamma_{i+1} \tilde{\gamma}_{i+1} l_i l_j l_{i+2} l_{j+2} + \gamma_{j+2} \tilde{\gamma}_{j+2} l_i l_j l_{i+1} l_{j+1} \right. \\ \left. - \gamma_{j+2} \tilde{\gamma}_{i+1} l_i l_j l_{i+2} l_{j+1} - \gamma_{i+1} \tilde{\gamma}_{j+2} l_i l_j l_{i+1} l_{j+2} \right]$$

$$= 2 \sum \left[ \gamma_i \tilde{\gamma}_i (l_{j+1}^2 + l_{j-1}^2) - \gamma_j \tilde{\gamma}_{j-1} l_j l_{j-1} - \gamma_j \tilde{\gamma}_{j+1} l_j l_{j+1} \right]$$

$$= 2 \sum_j \gamma_j \tilde{\gamma}_j, \quad \dots \quad (1.29)$$

$$\therefore \sum_j \gamma_j l_j = 0$$

$$[E = \frac{\mu}{2} \iint \gamma_{ij} \tilde{\gamma}_{ij} d\tau]$$

2. 速度場の表現 (以下  $U=1$  とする)

附録Aの核関数により同Bの可逆定理を用いると

$$u_j(Q) = \frac{1}{\mu} \iint_S \left[ \sum_i (u_i \tilde{T}_i^{(j)}) - \tau_i \tilde{U}_i^{(j)}(P, Q) \right] + \rho U \left( \sum_i u_i \tilde{U}_i^{(j)} \right) \frac{\partial x}{\partial n} \Big] dS(P), \quad (2.1)$$

なる表現を得る。

さて、 $S$ の内側で  $u_1 = -U$ ,  $u_2 = u_3 = 0$  なる速度場を考えると  
これについて上と同様な式が成立ち、かつ外側では0  
であるからそれを差引くと

$$u_j(Q) = \frac{-1}{\mu} \iint_S \sum_i \tau_i \tilde{U}_i^{(j)}(P, Q) dS(P), \quad \dots \quad (2.2)$$

のように簡単な表現が成立つ。

後の対称性から

$$\tilde{U}_i^{(j)}(P, Q) = U_i^{(j)}(Q, P), \quad \dots \quad (2.3)$$

であるから

$$u_j(Q) = -\frac{1}{\mu} \iint_S \sum_i \tau_i(P) U_i^{(j)}(Q, P) dS(P), \quad (2.4)$$

と書く事も出来る。

(附録Aの  $U_i^{(j)}(P, Q)$  であるから注意)

軸対称流れでは.

$$\begin{cases} u_2 \cos \theta + u_3 \sin \theta = u_r \\ -u_2 \sin \theta + u_3 \cos \theta = 0 \end{cases} \quad (2.5)$$

$$\bar{T}_1 = \frac{\mu}{r} \bar{T}_x, \quad \bar{T}_2 = \frac{\mu}{r} \bar{T}_r \cos \theta, \quad \bar{T}_3 = \frac{\mu}{r} \bar{T}_r \sin \theta,$$

よって

$$\begin{cases} u_1(Q) = - \int_C [\bar{T}_x V_1^{(1)}(Q,P) + \bar{T}_r V_r^{(1)}(Q,P)] dS(P), \\ u_r(Q) = - \int_C [\bar{T}_x V_1^{(r)}(Q,P) + \bar{T}_r V_r^{(r)}(Q,P)] dS, \end{cases} \quad (2.6)$$

$$\begin{cases} u_n = u_1 \cos \alpha + u_r \sin \alpha \\ u_s = -u_1 \sin \alpha + u_r \cos \alpha \end{cases}$$

$$\begin{cases} \bar{T}_n = \bar{T}_x \cos \alpha + \bar{T}_r \sin \alpha = -\frac{r}{\mu} p \\ \bar{T}_s = -\bar{T}_x \sin \alpha + \bar{T}_r \cos \alpha = \tau \end{cases} \quad (2.7)$$

よって

$$\begin{cases} u_n(Q) = - \int_C [\bar{T}_n U_n^{(n)}(Q,P) + \bar{T}_s U_s^{(n)}(Q,P)] dS, \\ u_s(Q) = - \int_C [\bar{T}_n U_n^{(s)}(Q,P) + \bar{T}_s U_s^{(s)}(Q,P)] dS, \end{cases} \quad (2.8)$$



$$\begin{aligned}
 U_n^{(n)} &= V_1^{(1)} \cos \alpha \cos \alpha' + V_r^{(1)} \sin \alpha \cos \alpha' + V_1^{(2)} \sin \alpha' \cos \alpha + V_r^{(2)} \sin \alpha \sin \alpha' \\
 U_s^{(2)} &= -V_1^{(1)} \sin \alpha \cos \alpha' + V_r^{(1)} \cos \alpha \cos \alpha' - V_1^{(2)} \sin \alpha \sin \alpha' + V_r^{(2)} \cos \alpha \sin \alpha' \\
 U_n^{(5)} &= -V_1^{(1)} \cos \alpha \sin \alpha' - V_r^{(1)} \sin \alpha \sin \alpha' + V_1^{(2)} \cos \alpha \cos \alpha' + V_r^{(2)} \sin \alpha \cos \alpha' \\
 U_s^{(5)} &= V_1^{(1)} \sin \alpha \sin \alpha' - V_r^{(1)} \cos \alpha \sin \alpha' - V_1^{(2)} \sin \alpha \cos \alpha' + V_r^{(2)} \cos \alpha \cos \alpha'
 \end{aligned}
 \tag{2.9}$$

## 3. 速度場の漸近性

レイノルズ数が充分小さいと (A.11) より,  $U_j^{(1)}$  は  
ストークス核  $U_{ij}^{(st)}$  に一致するので

$$u_j(Q) \stackrel{(1)}{\approx} -\frac{1}{\mu} \int_S \sum_i \tau_{ij} U_{si}^{(j)}(Q, P) dS_P, \quad \dots (3.1)$$

なおストークス核では

$$U_{si}^{(j)}(P, Q) = U_{si}^{(j)}(Q, P), \quad \dots (3.2)$$

である。

(2.4) において 完全遠方では

$$u_j(Q) \approx -\frac{1}{\mu} \sum_i X_i U_i^{(j)}(Q, 0), \quad \dots (3.3)$$

$$\text{但し} \quad X_i = \int_S \tau_i dS, \quad \dots (3.4)$$

軸対称流れでは  $X_2 = X_3 = 0$  故

$$u_j(Q) \approx -\frac{X_1}{\mu} U_1^{(j)}(Q, 0), \quad \dots (3.5)$$

附録 A の式より  $x$  軸の近傍で「上流側」では

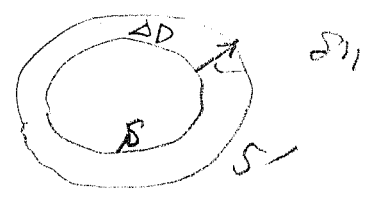
後流とは反対

ポアソニヤル流れとなり, 後流では wake を持つ。

4. 物体の微小変形 ( $U=1$  とする)

物体  $S$  が法線方向に僅かに  $\delta n$  だけ  $D' (= D - \Delta D)$

滑らかに変形し  $S'$  となったとする。  
 (領域は  $D$  から  $D'$  に変る)  
 速度場は  $(u_j)$  から  $(u'_j)$  に変化し



抵抗力は  $X_1$  から  $X'_1$  に変わったとしよう。

境界条件は

$$\left. \begin{aligned} u'_1 = -1, \quad u'_2 = u'_3 = 0 \\ \tilde{u}'_1 = 1, \quad \tilde{u}'_2 = \tilde{u}'_3 = 0 \end{aligned} \right\} \text{ on } S', \quad (4.1)$$

$$X'_1 = \iint_{S'} \tau'_i dS = -\rho \iiint_{D'} \tilde{u}'_j \frac{\partial u'_j}{\partial x} d\tau - E_{D'}(u'_j, \tilde{u}'_j), \quad (4.2)$$

( $d\tau \equiv dx dy dz$ )

$E$  の下添字は積分領域を意味する。

$$X_1 = \iint_S \tau_i dS = -\rho \iiint_D \tilde{u}_j \frac{\partial u_j}{\partial x} d\tau - E_D(u_j, \tilde{u}_j), \quad (4.3)$$

$$\delta X_1 = X'_1 - X_1 \equiv I - II, \quad (4.4)$$

$$I = E_{\Delta D}(u_j, \tilde{u}_j) + \rho \iiint_{\Delta D} \tilde{u}_j \frac{\partial u_j}{\partial x} d\tau, \quad (4.5)$$

$$\begin{aligned} II = E_D(\delta u_j, \tilde{u}_j) + E_D(u_j, \delta \tilde{u}_j) \\ + \rho \iiint_D \left[ \tilde{u}_j \frac{\partial \delta u_j}{\partial x} + u_j \frac{\partial \delta \tilde{u}_j}{\partial x} \right] d\tau, \end{aligned} \quad (4.6)$$

但し  $u'_j - u_j = \delta u_j$

$\Delta D$  は 充分小さいから近似的に (1.29) より

$$I = \sum_j \iint_S \left[ \mu \tilde{s}_j \tilde{s}_j + \rho \tilde{u}_j \frac{\partial \tilde{u}_j}{\partial x} \right] \delta n dS, \quad (4.7)$$

次に (B.3) より

$$II = - \sum_j \iint_S (\tilde{T}_j \delta \tilde{u}_j + \tilde{u}_j \delta \tilde{T}_j) dS, \quad (4.8)$$

となり, 更に (B.5) により,

$$\iint_S \tilde{u}_j \delta \tilde{T}_j dS = \iint_S \left[ \tilde{T}_j \delta \tilde{u}_j - \rho \tilde{u}_j \delta \tilde{u}_j \frac{\partial x}{\partial n} \right] dS, \quad (4.9)$$

(和記号は略す)

よって

$$II = - \iint_S (\tilde{T}_j \delta \tilde{u}_j + \tilde{T}_j \delta \tilde{u}_j - \rho \tilde{u}_j \delta \tilde{u}_j \frac{\partial x}{\partial n}) dS, \quad (4.10)$$

更に

$$\delta u_j = u_j'|_s - u_j|_s = - \frac{\partial u_j}{\partial n} \Big|_s \delta n, \quad (4.11)$$

であるから (1.20) より

$$\sum_j (\tilde{T}_j \delta \tilde{u}_j + \tilde{T}_j \delta \tilde{u}_j) = - 2\mu \left( \sum_j \tilde{s}_j \tilde{s}_j \right) \delta n, \quad (4.12)$$

よって

$$II = + \iint_S \left[ 2\mu \tilde{s}_j \tilde{s}_j - \rho \tilde{u}_j \frac{\partial \tilde{u}_j}{\partial x} \right] \delta n dS, \quad (4.13)$$

$$\therefore \delta u_j \frac{\partial x}{\partial n} = - \frac{\partial u_j}{\partial n} \frac{\partial x}{\partial n} \Big|_s \delta n = - \frac{\partial u_j'}{\partial x} \delta n, \quad (4.14)$$

$$\begin{aligned} \therefore \delta X_1 &= \sum_j \iint_S \left[ 2\rho \tilde{u}_j \frac{\partial u_j}{\partial x} - \mu \sum_j \tilde{s}_j \tilde{s}_j \right] \delta n dS, \quad (4.15) \\ &= \iint_S \left[ 2\rho \frac{\partial u_1}{\partial x} - \mu \sum_j \tilde{s}_j \tilde{s}_j \right] \delta n dS, \end{aligned}$$

同様に  
 $\tilde{u}_1 = \tilde{u}_1 - \tilde{u}_1 = -\tilde{I} + \tilde{II}$

$$\delta X_1^{\tilde{u}} = \tilde{X}_1^{\tilde{u}} - \tilde{X}_1^{\tilde{u}} = -\tilde{I} + \tilde{II}, \quad (4.16)$$

$$\tilde{I} = \iint_S \left[ \mu \sum_j \tilde{s}_j \tilde{s}_j + \rho \frac{\partial \tilde{u}_1}{\partial x} \right] \delta n dS, \quad (4.17)$$

$$\tilde{II} = \iint_S \left[ 2\mu \sum_j \tilde{s}_j \tilde{s}_j - \rho \frac{\partial \tilde{u}_1}{\partial x} \right] \delta n dS, \quad (4.18)$$

$$\delta X_1^{\tilde{u}} = \iint_S \left[ \mu \sum_j \tilde{s}_j \tilde{s}_j - 2\rho \frac{\partial \tilde{u}_1}{\partial x} \right] \delta n dS, \quad (4.19)$$

よって

$$\delta X_1 + \delta X_1^{\tilde{u}} = 2\rho \iint_S \frac{\partial}{\partial x} (u_1 - \tilde{u}_1) \delta n dS = 0, \quad (4.20)$$

$$(\because X_1 = \tilde{X}_1).$$

$$\begin{aligned} \frac{\delta X_1 - \delta X_1^{\tilde{u}}}{2} &= \delta X_1 = -\delta X_1^{\tilde{u}} \\ &= \iint_S \left[ \rho \frac{\partial}{\partial x} (u_1 + \tilde{u}_1) - \mu \sum_j \tilde{s}_j \tilde{s}_j \right] \delta n dS, \quad (4.21) \end{aligned}$$

軸対称流れでは (1.28) 等により

$$\left. \begin{aligned} \delta X_1 &= - \iint_S [\mu \tilde{S}^2 + 2\rho \tilde{S} r \sin \alpha \cos \alpha] \delta n dS \\ \delta X_2 &= - \iint_S [\mu \tilde{S}^2 + 2\rho \tilde{S} r \sin \alpha \cos \alpha] \delta n dS \end{aligned} \right\} \dots (F.22)$$

これは形式的に 2次元流れと全く同じであるため、  
最少抵抗問題についても全く同じ取扱が成り立つ。

# 附録 A 核関数

$$P_R(p, q) = \frac{\mu}{4\pi} \frac{\partial}{\partial x_j} \left( \frac{1}{R} \right), \quad R = \overline{PQ} = \sqrt{(x-x')^2 + (y-y')^2 + (z-z')^2}, \quad (A.1)$$

$$P \equiv (x, y, z), \quad Q \equiv (x', y', z')$$

$$U_j^{(k)} = \frac{1}{8\pi} \frac{\partial^2}{\partial x_j \partial x_k} \bar{\Phi} - \frac{\delta_{jk}}{8\pi} \Delta \bar{\Phi}, \quad (A.2)$$

$$\bar{\Phi} = \frac{1}{R} \int_0^{R(R-(x-x'))} \frac{1-e^{-\alpha}}{\alpha} d\alpha, \quad (A.3)$$

$$\Delta \bar{\Phi} = \frac{2}{R} e^{-R(R-(x-x'))}, \quad (A.4)$$

$$\Delta \bar{\Phi} - 2R \frac{\partial}{\partial x} \bar{\Phi} = \frac{2}{R}, \quad (A.5)$$

$\bar{\Phi}$  の微分を  $Q \equiv 0$  として下と

$$\bar{\Phi} = \frac{1}{R} \int_0^{R(R-x)} \frac{1-e^{-\alpha}}{\alpha} d\alpha + \frac{1}{R} \int_0^{\frac{\alpha^2}{4}} \left[ 1 - \frac{\alpha}{2} + \frac{\alpha^2}{6} \right] d\alpha$$

$$\stackrel{R \rightarrow 0}{=} (R-x) \left[ 1 - \frac{\alpha}{4} + \frac{\alpha^2}{18} + \dots \right], \quad \alpha = R-x$$

$$\bar{\Phi}_x = \left( \frac{x}{R} - 1 \right) \frac{1-e^{-R(R-x)}}{R(R-x)} \stackrel{R \rightarrow 0}{=} -\frac{1-e^{-R(R-x)}}{R^2} \stackrel{R \rightarrow 0}{=} \left( \frac{x}{R} - 1 \right), \quad (A.6)$$

$$\bar{\Phi}_y = \frac{y}{R} \frac{1-e^{-R(R-x)}}{R(R-x)} \stackrel{R \rightarrow 0}{=} \frac{y}{R}$$

$$\bar{\Phi}_z = \frac{z}{R} \frac{1-e^{-R(R-x)}}{R(R-x)} \stackrel{R \rightarrow 0}{=} \frac{z}{R}$$

$$\bar{\Phi}_{xx} = \frac{1}{R} \left( 1 - \frac{x^2}{R^2} \right) \frac{1-e^{-\alpha}}{\alpha} + R \left( \frac{x}{R} - 1 \right)^2 \left[ \frac{e^{-\alpha}}{\alpha} - \frac{1-e^{-\alpha}}{\alpha^2} \right]$$

$$\stackrel{R \rightarrow 0}{=} \frac{1}{R} \left( 1 - \frac{x^2}{R^2} \right) \left[ 1 - \frac{\alpha}{2} + \dots \right] + \frac{1}{R^2 R^2} \left[ -\frac{\alpha^2}{2} + \dots \right]$$

$$= \frac{1}{R} \left( 1 - \frac{x^2}{R^2} \right)^2$$

$$\frac{\partial \alpha}{\partial y} = \frac{k y}{r}$$

$$\bar{\Phi}_{xy} = -\frac{xy}{r^3} \left( \frac{1-e^{-\alpha}}{\alpha} \right) + \frac{ky}{r} \left( \frac{x}{r} - 1 \right) \left( \frac{e^{-\alpha}}{\alpha} - \frac{1-e^{-\alpha}}{\alpha^2} \right),$$

$$\bar{\Phi}_{xz} = -\frac{xz}{r^3} \left( \frac{1-e^{-\alpha}}{\alpha} \right) + \frac{kz}{r} \left( \frac{x}{r} - 1 \right) \left( \frac{e^{-\alpha}}{\alpha} - \frac{1-e^{-\alpha}}{\alpha^2} \right),$$

$$\bar{\Phi}_{yy} = \left( \frac{1}{r} - \frac{y^2}{r^3} \right) \left( \frac{1-e^{-\alpha}}{\alpha} \right) + \frac{ky^2}{r^2} \left( \frac{e^{-\alpha}}{\alpha} - \frac{1-e^{-\alpha}}{\alpha^2} \right),$$

$$\bar{\Phi}_{yz} = -\frac{yz}{r^3} \left( \frac{1-e^{-\alpha}}{\alpha} \right) + \frac{k y z}{r^2} \left( \frac{e^{-\alpha}}{\alpha} - \frac{1-e^{-\alpha}}{\alpha^2} \right),$$

$$\bar{\Phi}_{zz} = \left( \frac{1}{r} - \frac{z^2}{r^3} \right) \left( \frac{1-e^{-\alpha}}{\alpha} \right) + \frac{k z^2}{r^2} \left( \frac{e^{-\alpha}}{\alpha} - \frac{1-e^{-\alpha}}{\alpha^2} \right),$$

$$\frac{1-e^{-\alpha}}{\alpha} \doteq 1 - \left( 1 - \alpha + \frac{\alpha^2}{2} - \frac{\alpha^3}{6} \right) \doteq 1 - \frac{\alpha}{2} + \frac{\alpha^2}{6}$$

$$\frac{e^{-\alpha}}{\alpha} - \frac{1-e^{-\alpha}}{\alpha^2} = \frac{2}{\alpha^2} \left( \frac{1-e^{-\alpha}}{\alpha} \right) \doteq -\frac{1}{2} + \frac{\alpha}{3} + \dots$$

したがって

$$\Delta \bar{\Phi} - \frac{2}{R} \doteq 2k \bar{\Phi}_y = -\frac{2}{r} (1-e^{-\alpha}) \quad , \quad (A.8)$$

$$\begin{aligned} \text{又} \quad \bar{v}_{xx} &= \frac{1}{r} - \frac{x^2}{r^3}, & \bar{v}_{xy} &= -\frac{xy}{r^3}, & \bar{v}_{xz} &= -\frac{xz}{r^3} \\ \bar{v}_{yy} &= \frac{1}{r} - \frac{y^2}{r^3}, & \bar{v}_{yz} &= -\frac{yz}{r^3}, & \bar{v}_{zz} &= \frac{1}{r} - \frac{z^2}{r^3} \end{aligned} \quad (A.9)$$

したがって、ストークス流れの積を

$$U_{ij}^{(k)} = \frac{1}{8\pi} \frac{\partial^2}{\partial x_i \partial x_j} (R) - \frac{\delta_{ij} k}{4\pi R} \quad (A.10)$$

とすると

$$\begin{aligned} U_{ij}^{(k)}(P, Q) - U_{ij}^{(k)}(P, R) &= \frac{1}{8\pi} \frac{\partial^2}{\partial x_i \partial x_j} [\bar{\Phi} - R] \\ &\quad - \frac{\delta_{ij} k}{8\pi} [\Delta \bar{\Phi} - \frac{2}{R}] \quad (A.11) \end{aligned}$$

よって右辺は  $P \rightarrow Q$  で常に 0 となる。つまりストークス流れ一致である。



$$V_i^{(1)} = \int_0^{2\pi} U_i^{(1)} d\theta = \frac{1}{8\pi} \frac{\partial^2}{\partial x^2} \int_0^{2\pi} \bar{\Phi} d\theta - \frac{1}{8\pi} \int_0^{2\pi} \Delta \bar{\Phi} d\theta, \quad (A-12)$$

$$V_r^{(1)} = \int_0^{2\pi} (U_2^{(1)} \cos\theta + U_3^{(1)} \sin\theta) d\theta$$

$$= \frac{1}{8\pi} \int_0^{2\pi} d\theta \left[ \frac{\partial^2}{\partial x \partial r} \bar{\Phi} \right]$$

$$V_i^{(1r)} = \int_0^{2\pi} [U_1^{(2)} \cos\theta' + U_1^{(3)} \sin\theta'] d\theta' = \frac{1}{8\pi} \int_0^{2\pi} \frac{\partial^2}{\partial x \partial r'} \bar{\Phi} d\theta',$$

$$V_r^{(1r)} = \int_0^{2\pi} d\theta' \left[ \{U_2^{(2)} \cos\theta + U_3^{(2)} \sin\theta\} \cos\theta' + \{U_2^{(3)} \cos\theta + U_3^{(3)} \sin\theta\} \sin\theta' \right]$$

$$= -\frac{1}{8\pi} \int_0^{2\pi} d\theta \left[ \Delta \bar{\Phi} \cos(\theta - \theta') \right]$$

$$+ \frac{1}{8\pi} \int_0^{2\pi} d\theta' \left[ \frac{\partial^2 \bar{\Phi}}{\partial y \partial r'} \cos\theta' + \frac{\partial^2 \bar{\Phi}}{\partial z \partial r'} \sin\theta' \right]$$

$$= -\frac{1}{8\pi} \int_0^{2\pi} \Delta \bar{\Phi} \cos(\theta - \theta') d\theta' = \frac{1}{8\pi} \int_0^{2\pi} \frac{\partial^2 \bar{\Phi}}{\partial r' \partial r} d\theta', \quad (A-13)$$

$$\bar{\Phi}_{xr} = -\frac{(x-x')}{R^3} (r-r' \cos\theta\theta') \left( \frac{1-e^{-\alpha}}{\alpha} \right) + \frac{r(r-r' \cos\theta\theta')}{R} \left( \frac{x+x'}{R} - 1 \right) \left( \frac{e^{-\alpha}}{\alpha} - \frac{1-e^{-\alpha}}{\alpha^2} \right)$$

$$R^2 = (x-x')^2 + r^2 + r'^2 - 2rr' \cos(\theta - \theta'),$$

$$\bar{\Phi}_r = \frac{\{r - r' \cos(\theta - \theta')\}}{R} \left( \frac{1 - e^{-\alpha}}{\alpha} \right), \quad (A-14)$$

$$\bar{\Phi}_{rr'} = \left\{ \frac{-\cos(\theta - \theta')}{R} - \frac{\{r - r' \cos(\theta - \theta')\} \{r' - r \cos(\theta - \theta')\}}{R^3} \right\} \left( \frac{1 - e^{-\alpha}}{\alpha} \right)$$

$$+ \frac{R \{r - r' \cos(\theta - \theta')\} \{r' - r \cos(\theta - \theta')\}}{R^2} \left\{ \frac{e^{-\alpha}}{\alpha} - \frac{1 - e^{-\alpha}}{\alpha^2} \right\},$$

$R \rightarrow \infty$  の場合

$$e^{-k[R-(x-x')]} \doteq \begin{cases} 0 & \text{for } x \ll x' \\ e^{-\frac{k\omega^2 z}{2R}} & \text{for } x \gg x', \omega^2 = (y-y')^2 + (z-z')^2 \end{cases} \quad (A-15)$$

また  $x' \gg x$  (図 2 の後流側) では

$$\bar{\Phi}_{xx} \doteq \frac{\{R+(x-x')\}}{kR^3} - \frac{1}{kR^2} = \frac{y-x'}{kR^3}$$

$$\bar{\Phi}_{xy} \doteq -\frac{(x-x')(y-y')}{kR^3(R-x-x')} + \frac{(y-y')}{kR^2(R-x-x')} \doteq \frac{y-y'}{2kR^3} \left(1 - \frac{x-x'}{R}\right) \doteq \frac{y-y'}{kR^3}$$

$$\bar{\Phi}_{xz} \doteq -\frac{(x-x')(z-z')}{kR^3(R-x-x')} - \frac{(z-z')}{kR^2(R-x-x')} \doteq -\frac{z-z'}{kR^3}$$

$$\bar{\Phi}_{yy} \doteq \frac{R^2 - (y-y')^2}{kR^3(R-x-x')} - \frac{(y-y')^2}{kR^2(R-x-x')^2} \doteq \frac{1}{2kR} - \frac{3(y-y')^2}{4kR^4} \quad (A-16)$$

$$\bar{\Phi}_{yz} \doteq -\frac{(y-y')(z-z')}{kR^3(R-x-x')} \left[1 + \frac{R}{R-x}\right] \doteq -\frac{3(y-y')(z-z')}{4kR^4}$$

$$\bar{\Phi}_{zz} \doteq \frac{1}{2kR} - \frac{3(z-z')^2}{4kR^4}$$

$$\nabla^2 \bar{\Phi} \doteq 0$$

$x \gg x'$  では wake が解る。 ...

## 附録 B 可逆定理

任意の速度場  $u_j$  と  $\tilde{u}_j$  に関する次の積分

$$E(u_j, \tilde{u}_j) = \frac{\mu}{2} \iiint_D \left[ \sum_i \sum_j \gamma_{ij} \dot{\gamma}_{ij}^{\tilde{u}} \right] dx dy dz, \quad \dots (B.1)$$

は可逆的, つまり  $u_j$  と  $\tilde{u}_j$  を入れかえても値は変わらない。

$$E(u_j, \tilde{u}_j) = E(\tilde{u}_j, u_j), \quad \dots (B.2)$$

部分積分して (1.1), (1.2) を使うと

$$E = -\rho U \iiint_D \left[ \sum_j \tilde{u}_j \frac{\partial u_j}{\partial x} \right] dx dy dz - \iint_S \left[ \sum_j \tilde{u}_j \tau_j \right] dS, \quad (B.3)$$

あるいは (1.4), (1.5) を使うと

$$E = \rho U \iiint_D \left[ \sum_j u_j \frac{\partial \tilde{u}_j}{\partial x} \right] dx dy dz - \iint_S \left[ \sum_j u_j \tau_j^{\tilde{u}} \right] dS, \quad (B.4)$$

すなわち (B.2) により

$$\iint_S \left[ \sum_j (\tilde{u}_j \tau_j - u_j \tau_j^{\tilde{u}}) \right] dS = -\rho U \iiint_D \left[ \sum_j \left( \tilde{u}_j \frac{\partial u_j}{\partial x} + u_j \frac{\partial \tilde{u}_j}{\partial x} \right) \right] dx dy dz = -\rho U \iint_S \left( \sum_j u_j \tilde{u}_j \right) \frac{\partial x}{\partial n} dS, \quad (B.5)$$

特に (1.6) (1.7) の境界条件を満足する流れで, 物体が用いていけば"右辺は消えて"

$$U \iint_S \tau_j dS = -U \iint_S \tilde{\tau}_j dS, \quad \dots (B.6)$$

となって 抵抗力は逆流れの, 元の流れの力の反対等しい。

(B.3), (B.4) により

$$\bar{H}(u_j, \tilde{u}_j) = \rho U \iiint_D \sum_i u_i \frac{\partial \tilde{u}_i}{\partial x} dx dy dz, \quad (\text{B.7})$$

表面積分を導入すると

$$\begin{aligned} E(u_j, \tilde{u}_j) &= \bar{H}(u_j, \tilde{u}_j) + \iint_S \sum_i u_j \tilde{T}_i ds \\ &= -\bar{H}(\tilde{u}_j, u_j) + \iint_S \sum_i \tilde{u}_j T_i ds, \quad (\text{B.8}) \end{aligned}$$

$$\bar{H}(u_j, \tilde{u}_j) + \bar{H}(\tilde{u}_j, u_j) = \rho U \iint_S \left( \sum_i u_j \tilde{u}_j \right) \frac{\partial x}{\partial n} dS, \quad (\text{B.9})$$

↑  
sign?